PHYSICAL AND DYNAMICAL STUDIES OF METEORS

Contract NAS 1-11204

Special Progress Report

1 February to 30 November 1973

Principal Investigators

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June 1974

(NASA-CR-132534) PHYSICAL AND DYNAMICAL N75-10891 STUDIES OF METEORS Special Progress Report, 1 Feb. - 30 Nov. 1973 (Smithsonian Astrophysical Observatory) Unclas 38 p HC \$3.75 CSCL 03B G3/91 53194

Prepared for

National Aeronautics and Space Administration
Langley Research Center
Langley Station
Hampton, Virginia 23365

Smith sonian Institution Astrophysical Observatory Cambridge, Massachusetts 02138

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1. Report No. NASA CR-132535	2. Government Acces	ssion No.	3. Re	cipient's Catalog No.			
4. Title and Subtitle	Title and Subtitle PHYSICAL AND DYNAMICAL STUDIES OF METEORS						
PHISICAL AND DYNAMICAL SID	DIES OF METEORS		6. Pe	forming Organization Code			
7. Author(s) Richard B. Southworth and	8. Pe	forming Organization Report No.					
Q. Porforming Operation No.	d	<u></u>	10. Wo	rk Unit No.			
 Performing Organization Name and Ad- Smithsonian Institution, A 		nrv		B-45-52-03			
Cambridge, Massachusetts	02138	:	NA.	ntract or Grant No. 51-11204			
12. Sponsoring Agency Name and Address	s ,		-	pe of Report and Period Covered itractor Report			
National Aeronautics and S Washington, DC 20546	pace Administration			onsoring Agency Code			
15. Supplementary Notes							
This is a topical report							
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 Key Words (Suggested by Author(s)) pobservation, distributions space density; fragmentation; masses; orbital parameters observation; image orthicol 	; selection effects; on; meteor streams; diffusion; meteor ; simultaneous	18. Distribution Statement Unclassified - Unlimited					
9. Security Classif. (of this report)	20. Security Classif, (of this	page)	21. No. of Pages	22. Price*			
Unclassified	Unclassified		35	\$3.25			

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PHYSICAL AND DYNAMICAL STUDIES OF METEORS

Special Progress Report

1. SPACE DENSITY AND COLLISIONS OF METEOROIDS

A revised version of Sections 6 and 7 of our previous Special Progress Report (NASA CR-2316) is being prepared for journal publication.

A general theoretical investigation of space density of meteoroids, which takes collisions, the Poynting-Robertson effect, and sources into account, has been formulated. It will be carried further when the observational bias resulting from fragmentation has been quantitatively assessed.

2. FRAGMENTATION

2.1 Significance of Fragmentation

Jacchia (1955) showed that mass ablation in the form of small particles, rather than in that of individual molecules, predominates in the fainter photographic (Super-Schmidt) meteors. Fragmentation of this sort was, naturally, expected in radar meteors; finally, Southworth (1973) showed that it is common in the Havana radar meteors. Theoretical treatments of the physical interaction of the meteoroid with the atmosphere have not yet, however, properly come to grips with the physics of fragmentation.

A study of fragmentation was included in the present program of research for several reasons: The synoptic-year data, because of the careful calibration of the Havana recording apparatus, contains more information on radar meteor fragmentation than has hitherto been available. A better understanding of the physical interaction is essential for proper interpretation of the observations, especially as regards selection effects (the possible drastic selection effect that depends on fragmentation is discussed below). Finally, we hope to learn more about the physical nature of the meteoroid before it enters the atmosphere.

The present discussion is of the nature of an interim report on an uncompleted study. It will, however, permit some useful conclusions to be accepted temporarily.

2.2 Data

This report uses the condensed results of the synoptic-year reductions; specifically, some of the results for each meteor that were originally designed to be punched on "height-density cards," and that are now on tape. The detailed results for individual meteors, originally designed to be printed, have not

been used because the computer programing to transform tape designed for printing to tapes suitable for machine reading is not yet complete.

From the synoptic year, 3550 meteors with well-defined decelerations and ionization curves were selected.

As usual in this project, linear electron densities in the ionized column have been denoted by radar magnitudes as defined by Kaiser's (1955) relation,

$$M = 35 - 2.5 \log_{10} q , \qquad (1)$$

where q is electrons per centimeter. The computer performs a least-squares fit of the magnitudes M_i deduced from the initial Fresnel zones at stations i and the times t_i of crossing the specular reflection points to a quadratic

$$M_i = a t_i^2 + b t_i + c$$
 (2)

which represents the ionization curve. If this curve indicates a maximum of ionization (rather than a minimum) and if the distribution of stations along the ionization curve reached close enough to the ends (defined by the limiting observable magnitude), the curve is taken to be well defined. The beginning and end heights above sea level h_B and h_E are defined by the points where the ionization curve reached limiting magnitude. The height of maximum ionization h_M is halfway between h_B and h_E, since the observations would only rarely admit a more elaborate form than equation (2). Decelerations were taken to be well defined if positive, and larger than 0.4 of their standard errors. Diffusion rates were also required to be consistent between observations at different stations.

Preatmospheric masses m_{∞} have been revised from the computer outputs, by using the ionizing efficiencies found from simultaneous radar-television observations (Cook et al., 1973). Observed ablation coefficients σ were computed with values at the maximum of the ionization curve

$$\sigma = \frac{\dot{m}_{max}}{(m_{max} v_{max} \dot{v}_{max})},$$
(3)

where the mass-loss rate m is computed from maximum electron density, and the mass at maximum ionization is taken to be

$$m_{\max} = \frac{m_{\infty}}{2} . \tag{4}$$

For use in subsequent analysis, "effective" fragment masses m_f and "effective" numbers of fragments N_f have been computed as follows. The computer output gives the "apparent" density δ of a spherical meteoroid that would experience the observed deceleration on the simplified single-body theory (Hawkins and Southworth, 1958). This has been revised by use of the radar—television ionizing efficiency. (The provisional use in the reductions of CIRA 1961 atmospheric densities and the values $\Gamma = A = 1$ for the drag coefficient and shape factor may require much smaller revisions in the future.) If the meteor is conceptually replaced by N_f equal spherical fragments of density 3.4 g cm⁻³, which would each exhibit the observed deceleration and which sum to the observed mass, we have

$$N_{f} = \left(\frac{3.4}{\delta}\right)^{2} \tag{5}$$

and

$$m_{f} = \frac{m_{\text{max}}}{N_{f}} . ag{6}$$

Density 3.4 is taken here, of course, because it is the approximate value for stony meteorites.

Table 1 includes a variety of data for these 3550 meteors. They have been divided into groups of preatmospheric mass m_{∞} and deceleration v_{\max} at the point of maximum ionization. (v_{\max} is not the maximum deceleration,

which occurs near the end.) The division into groups of m is also almost an exact division into groups of velocity v at the point of maximum ionization, because of the limited dynamic range of the radar receivers, and the very steep dependence of ionizing efficiency on velocity. Successive lines of the table give 1) range of $\dot{\mathbf{v}}_{\text{max}}$ (km sec⁻²), 2) range of $\mathbf{m}_{\infty}(\mathbf{g})$, 3) fraction of the 3550 meteors with these $\hat{\mathbf{v}}$ and \mathbf{m}_{∞} , 4) mean value of \mathbf{v}_{\max} , 5) mean value of v_{max}, 6) mean number of Fresnel pattern extrema observed, 7) logarithmic mean of effective mass of a fragment (g), 8) logarithmic mean of effective number of fragments, 9) distribution of mean numbers of extrema: 4 lines show, respectively, the fractions of the group with 5-7, 8-12, 13-19, and 20-30 extrema observed, 10) distribution of logarithms of effective. fragment masses: 5 lines show, respectively, the fractions whose logarithm of mass (g) is (>-4), (\leq -4 and >-5), (\leq -5 and >-6), (\leq -6 and >-7), and (≤-7), 11) distribution of logarithms of effective number of fragments: 5 lines show, respectively, the fractions whose logarithm of effective number of fragments is (<0), (≥ 0 and <2), (≥ 2 and <4), (≥ 4 and <6), and (≥ 6), 12) height of maximum ionization (km), 13) trail length (km), 14) rise above limiting magnitude M_{lim} - M_{max}, 15) maximum magnitude, 16) logarithm of ablation coefficient (cgs). Logarithms are decimal. Groups containing fewer than 10 meteors (less than a fraction 0.0028 of the sample) have not been listed, but are represented in the sum groups. The average of the logarithm of preatmospheric mass is not tabulated, but may be found as the sum of the averages of logarithms of effective fragment mass and number of effective fragments. There are no observations of large meteors with large deceleration or small meteors with small deceleration in Table 1. Any analysis of fragmentation needs to explain this absence.

2.3 Height Data

Our observable meteor heights are known to be bounded on the top by diffusion (Southworth, 1973). This is inevitably reflected in the selection of data for Table 1, although the effect is much smaller there than in the total observational sample because high meteors are much less likely to have their deceleration sufficiently well measured for Table 1. An unbiased determination

of the trend of heights with velocity can be derived from Figure 4-1 of Southworth and Sekanina (1973). Because the diffusion limit to height increases with velocity, some observations are missed at all velocities but the effect is marked only at the highest velocities. Taking the peaks of the height histograms in Figure 4-1 and adding estimated corrections of 2 km to the height at the highest velocity group and 1 km to the height at the next two velocity groups, we derive Figure 1.

The straight line drawn in Figure 1 corresponds to the following relation between the atmospheric density ρ_{\max} at the point of maximum ionization and the velocity v,

$$\rho_{\text{max}} \propto v^{-1.9} \tag{7}$$

2.4 Fresnel Pattern Extrema

Successive maxima and minima (collectively extrema) of the observed Fresnel diffraction patterns are formed by the passage of the head of the ionized column across successively shorter intervals (Fresnel zones) of the trail. The time interval between successive extrema decreases uniformly, and the difference in amplitude decreases monotonically (often until there are no further extrema), so that only a rather well-defined number of extrema can be measured. We will interpret this number in terms of fragmentation, but it is first necessary to discuss other effects.

The computer program that found the extrema rejected data yielding fewer than 5 extrema, and stopped its search at 30. However, extrapolation of the distribution of the mean number of extrema measured per meteor (MEXT in Table 1) shows that the data lost by both limits is relatively small. The loss is not important for the analysis in this report and can be taken into account elsewhere. The computer program also stopped its count of extrema whenever the interval between successive extrema decreased below 1.5 radar pulses, to avoid misidentifications. At the mean velocity and slant range of each of the mass groups in Table 1, this limits the observed number of extrema to

the values given in Table 2. The breakdowns of MEXT in Table 1 show that some meteors in each group had more observed extrema than the limit for the mean; these are meteors at greater than mean range or less than mean velocity. Correspondingly, other meteors would have had lower limits to observed extrema. The mean number of observed extrema is significantly below the limit imposed by the 1.5-pulse spacing (and below the limit of 30 extrema). We conclude that the 1.5-pulse spacing limit is responsible for much of the difference in mean number of extrema observed at different masses and velocities, but that other limitations are common.

Diffusion of the ion column into the surrounding atmosphere causes an exponential decay in the smoothed (Fresnel oscillations removed) amplitude, which eliminates extrema after an initial few. We may study this in terms of Loewenthal's (1956) theoretical Fresnel patterns, which depend on his parameter

$$C = \frac{8\pi D\sqrt{\lambda R/2}}{\lambda^2 v} , \qquad (8)$$

where D is the diffusion coefficient, λ the radar wavelength, and R the slant range. Within our observed height interval,

$$\log_{10} D(cm^2 sec^{-2}) = 0.068h - 1.67$$
 (9)

where h is height in kilometers. We may take mean slant range to be twice mean height adequately for this purpose. Table 2 also gives C computed by use of mean velocity and height for each group in Table 1. Values of C below 0.29 eliminate no extrema before the 30th, and the values of C just found have no practical effect on the ease of observing any extremum. There are, of course, meteors at greater heights than the mean that are more affected by diffusion, but the restriction in Table 1 to meteors giving good decelerations essentially eliminates all those close to the diffusion ceiling on height. We conclude that diffusion is unimportant in determining the observed numbers of extrema in Table 1.

The remaining possible limitation to observed numbers of extrema is fragmentation. Arbitrary distributions of fragments along the trajectory can give very odd Fresnel patterns, but any reasonably smooth unimodal distribution suppresses, or nearly suppresses, all Fresnel oscillations after the interval between two successive maxima or minima has shrunk to the whole half-width of the fragment distribution. Attributing much of the limitation on extrema to fragmentation, we interpret the width of the last two observed Fresnel zones as a high estimate of the half-width of the fragment spread. If k extrema were observed, the width of the last two zones is, very nearly,

$$w = \sqrt{\frac{R\lambda}{2(k-3/4)}} \quad , \tag{10}$$

and again we may take R to be twice the height for this purpose. Table 2 gives values of w, computed with mean values of k and height.

2.5 Lag

Observed distances between radar meteor fragments much exceed the fragment diameters and atmospheric mean free paths, and are very nearly parallel to the direction of motion. We infer that the fragments are independent of each other when observed, and that we may neglect any aerodynamic interaction between fragments after their initial separation. It is natural to compare the relative displacements of the fragments along the trajectory with the total displacement of the main body or of the center of the group of fragments caused by the atmosphere. This total displacement will be called the "lag;" it is the distance between the main body (or fragment group) and a hypothetical meteoroid that has experienced no atmospheric deceleration since the fragments separated. A fragment whose mass/cross-section ratio is 1/f of the mass/cross-section of the main body would be expected to have f times the lag of the main body.

The distribution of mass/cross-section among fragments in a group depends on their mass, shape, and density distributions. It cannot be predicted with any certainty, but an attempt (too long to describe here) at a

realistic estimate concludes that the standard deviation of mass/cross-section is roughly 0.3 to 0.5 of the mean value.

If separation occurs at t_0 , and if $\dot{\mathbf{v}}$ is the meteoroid deceleration, the lag at time t is

$$L = -\int_{t_0}^{t} \int_{t_0}^{t_2} \dot{v} dt_1 dt_2 . \qquad (11)$$

The observed values of v_{max} in Table 1 were derived by fitting observed velocities v at times t to an expression equivalent to

$$v = v_{max} - v_{max} \{ exp[1.4 v_{max} cos Z_R H^{-1} (t - t_{max})] - 1 \}$$
 (12)

Without the factor 1.4, and provided the v_{max} term is relatively small, (12) is the theoretical form for the deceleration of a nonablating single meteoroid in an exponential atmosphere. The empirical factor 1.4, adopted from the results of Super-Schmidt meteors, roughly adapts the form to ablation and fragmentation. Nothing more refined is possible with the radar data.

The time of fragment separation is of course unknown, but we will temporarily assume that separation occurs at the beginning of the observed ionized trail. By use of (11) to approximate v, and neglecting $1 - v/v_{\rm max}$, the lags at the maximum and end of the ionized trail are

$$L_{\text{max}} = -\left(\frac{G}{v_{\text{max}}}\right)^2 v_{\text{max}} \left[1 - \left(1 + \frac{g}{2G}\right) \exp\left(\frac{-g}{2G}\right)\right]$$
 (13)

and

$$L_{end} = -\left(\frac{G}{v_{max}}\right)^2 \dot{v}_{max} \exp\left(\frac{g}{2G}\right) \left[1 - \left(1 + \frac{g}{G}\right) \exp\left(\frac{-g}{G}\right)\right] , \quad (14)$$

where g is the trail length and

$$G = H/1.4 \cos Z_{R} \tag{15}$$

is the scale distance in which deceleration increases by a factor e. Substituting mean values of $\cos Z_R = 0.7$ and H = 6, and v_{max} and g from Table 1, we obtain the representative values of L_{max} and L_{end} shown in Table 3.

2.6 Fragmentation Degrades Observed Decelerations

Table 3 also contains the width w of the last two observed Fresnel zones. Taking w as a high estimate of the fragment spread, we expect it to be roughly proportionate to the lag. It is evident, however, that this is not true; the lag (either one) is proportional to deceleration but w is almost independent of deceleration.

We resolve the problem by observing that a group of fragments some 200 m long is not as satisfactory a radar target as the single body on which the analyses have been founded. The centroid of the group will shift within the group as different fragments increase or decrease their electron output. Any spread of the fragments normal to the trajectory, moreover, will have a very large effect on the centroid; we will neglect this effect for the present. The fragments will tend to be arranged in rough order of ablation, the most recently ablated being at the head. If the meteoroid is inhomogeneous in structure, we may expect systematic differences in fragment size within the group, and therefore large shifts in the radar centroid as one subgroup or another flares (subfragments) or burns out.

To estimate a plausible "fragmentation" error in deceleration, consider a 100-m shift of the radar centroid within the 200-m group while one Fresnel pattern is generated (typically 2 to 3 km of trajectory). That pattern would imply a velocity 3 to 5% wrong. The typical drop in velocity between the first and last observed Fresnel patterns is 8%, virtually independent of velocity. In a simple case, where the erroneous velocity is one of only two velocities with significant weight, one at the beginning and one at the end, the centroid

shift thus causes a deceleration error of the order of 40 to 60%. There are comparable errors in other cases. A back-and-forth shift of the centroid would obviously cause even larger errors.

Confirmation of the unreality of the "observed" decelerations is given by the near independence of height and deceleration within each mass group of Table 1. Any real physical circumstance causing order-of-magnitude differences in deceleration ought to have more effect on height. We would, furthermore, expect deceleration to be proportional to the cosine of the radiant zenith distance $\cos Z_R$, but that quantity (not tabulated here) shows only the most moderate trend toward larger values at the higher decelerations.

Once the fragmentation error in deceleration is recognized, we see that individual decelerations are of small value and that we should confine further interest in Table 1 to the right-hand column, which is an average of the others. Conversely, being convinced that the scatter in the decelerations is largely unreal, we deduce the probable inhomogeneity of the meteoroids, since \log_{10} (number of fragments) ranges from 0.8 to 1.4 in Table 1, and random electron-output variations among so many fragments would not shift the group centroid enough to cause the observed deceleration scatter.

2.7 Trail Lengths

The 11-km spacing between stations was chosen to obtain well-distributed observations along some of the longer ionized trails we expected to record. This expectation was based on the simplified theory for single-body meteoroids as well as on observed trail lengths for bright radar meteors, but it proved wrong for the faint radar meteors recorded at Havana. These, we found, typically had much shorter trails. Well-distributed observations by five or six stations were indeed common, but only when the meteor's path lay more nearly perpendicular than parallel to the line of five stations.

The simplified single-body theory (Hawkins and Southworth, 1958) made the vertical length of the observable trail, h beg - h end, dependent only on the

difference between the maximum and limiting magnitudes, $M_{lim} - M_{max}$. Table 4 shows theoretical lengths, observed lengths for faint photographic meteors, and lengths for a sample of 6803 synoptic-year meteors with well-defined ionization curves. A scale height H = 5.4 km is assumed for the theory. The standard deviation of a single radar trail length from the mean is designated σ_1 .

Table 4 shows that both photographic and radar trails are much shorter than the simplified theory. The most significant comparison between photographic and radar is for the magnitude difference interval 2-4. In the 0-2 interval, the radar data, unlike the photographic, are closely bunched to $M_{lim} - M_{max} = 2$. When $M_{lim} - M_{max} > 4$, the quadratic fit to the ionization curve is likely to be a poor extrapolation at M_{lim} .

Table 5 and Figure 2 show the relation between vertical trail length and $\cos Z_R$ for the same 6803 meteors. Quite unlike the simplified theory, we find that the actual (slant) trail length is much more nearly constant than is the vertical trail length. The data can be fitted approximately by

$$h_{\text{beg}} - h_{\text{end}} = 10.7 (\cos Z_R)^{0.89}$$
 (16)

(Note added in proof: We have just realized that the result in equation (16) is affected by systematic error, because the radar system is not oriented to observe long trails from meteors with small $\cos Z_R$. Nonetheless, the vertical trail length is still significantly dependent on $\cos Z_R$. Our best present assessment is that the use of (16) in the following section remains valid.)

2.8 Model for the Fragmentation Process

The Super-Schmidt observations introduced the concept of a meteoroid main body gradually shedding fragments (seen as the "wake") and sometimes entirely breaking up into an elongated cloud of fragments (seen as "terminal blending"). We use the same concept here for the radar meteors. Both the main body and fragments are considered to generate light and electrons.

Disentangling the effects of simultaneous fragmentation and ionization will not be easy. It is therefore worth noting that an alternative theory can be formed and to show why it fails. The alternative is to suppose that fragmentation occurs appreciably before ionization, so that single-body theory can be used for the (presumably solid) ionizing fragments. Several authors have treated small single bodies; their ionization curve is shorter at the beginning than the simplified theory because the heated outer layer is most of or all the body, and it may be shorter at the end because of deceleration, but it is not very different from the simplified theory. The ablation of fragments from the main body would be separately treated. It would have been convenient to use single-body theory here as well, in terms of a heat of fragmentation that is much smaller than the heat of vaporization in the usual theory, but that is ruled out by the ionization curves that are so much shorter than solid singlebody curves. The ionization curve of the fragment cloud must be at least as long as the curve for a single fragment and, if the fragments are all the same size or random sizes, at least as long as the "fragmentation curve" of the main body. (If large fragments are ablated first, and then smaller ones, it is possible for the fragment cloud's ionization curve to be shorter than the main body's fragmentation curve.) Nonetheless, while this model may be useful in clarifying ideas, it cannot be correct because of the marked dependence (equation 16) of vertical trail length on cos Zp; this is quite at variance with the trail lengths of solid single fragments.

We therefore turn to a model involving simultaneous fragmentation and ionization. The newly ablated fragments will enter the atmosphere at lower heights than they would have reached in independent fall; this is Öpik's (1958) "abnormal environment." Consequently, they will often have very short ionization curves, resembling the lower ends of normal ionization curves. A schematic ionization curve of the entire assembly of main body and fragments can neglect direct ionization by the main body, which will have a much smaller surface area than the fragments together. Two extreme cases of the model will help to clarify ideas. 1) If the main body breaks completely into many fragments before it has ablated appreciable mass by vaporization, we observe only the fragment cloud, and the ionization curve is that of the fragments, perhaps lacking the beginning. 2) If the main body ablates fragments so deep in the atmosphere that they have only very short ionization curves, the observed ionization curve is essentially the main body's fragmentation curve. The observed deceleration in case 1) is that of the fragments; in

2), that of the main body. In intermediate cases, it will tend to lie between those, but it is not difficult to construct cases (as in Section 2.6) where the observed deceleration is much smaller or larger than either the main body or the fragments.

Our working model for analysis of individual meteors is that our data represents a gradation from nearly case 1) for the low-mass (fast) meteors to nearly 2) for the high-mass (slow) meteors. In either event, the fragmentation curve is short compared to single-body ablation curves and, thus, cannot represent ablation of successive layers of fragments but something closer to a sudden collapse, where ablation of the first few fragments weakens the remaining structure. Only such a collapse combined with very short ionization curves for the fragments can explain the result in equation (16).

Our low-mass (fast) meteors appear to approach case 1) because the observed value of $\sigma \sim 10^{-12}$ matches that observed for large solid meteoroids. The relatively large fragment spread (~ 0.3 km) also appears to require fragmentation early in the ionization curve. Our high-mass (slow) meteors appear to approach case 2) because their observed $\sigma \sim 10^{-11}$ matches that observed for Super-Schmidt meteors where the main body and "wake" (fragment tail) can be separately observed. The greater trail length of the high-mass meteors is consistent with longer persistence of the main body than in low-mass meteors. The smaller fragment spread (~ 0.2 km) is also consistent.

2.9 Fragment Mass

Whatever the uncertainty in the fragmentation curve of the main body, we may identify the end of the observed ionization curve with the end of the fragment ionization curves. The simplified single-body theory predicts that the atmospheric density at any definite height interval before the end of the ionization curve, like that at the maximum, obeys

$$\rho \propto v^{-2} m_f^{1/3} , \qquad (17)$$

where m is the mass at the same height. Correcting (8) for the difference in trail length between fast and slow meteors, we find the atmospheric density at the end of the ionized curve to be

$$\rho_{end} \propto v^{-2.1}$$
 (18)

where the fragment mass, formally, obeys

$$m_f \propto v^{-0.3}$$
 (19)

Equation (19) should be regarded with caution. Because of our observational correlation between v and m, (19) could also be, roughly,

$$m_f \propto m^{0.04}$$
 (20)

and it is not yet clear that either exponent is significantly different from zero.

Table 1 gives mean effective fragment masses m_f . For the low-mass meteors, case 1) implies that this is the real fragment mass. For case 2), this would be $(\delta/3.4)^2$ m, where the total mass m is essentially the main body mass. For transitional cases, m_f would be somewhere between $(\delta/3.4)^2$ m and the fragment mass, thus considerably above the fragment mass. The values in Table 1 are therefore consistent with our finding that fragment mass is independent of velocity, and we find

$$m_f \sim 10^{-6} g$$
 . (21)

This is, furthermore, consistent with McCrosky's (1958) values of 10^{-4} to 10^{-6} g and Smith's (1954) value of 5×10^{-6} g for the masses of particles released in flares of photographic meteors, especially if equation (20) is correct in suggesting larger fragments from larger meteors.

2.10 Selection Effect of Fragmentation

The simplified theory predicts that deceleration at maximum ionization is nearly independent of velocity,

$$\dot{\mathbf{v}}_{\text{max}} \approx \frac{3 \cos Z_{\mathbf{R}}}{2H\sigma} \qquad (22)$$

where H is the atmospheric scale height (Hawkins and Southworth, 1958). Similarly, any model where σ is independent of velocity (as seems to be the case for the photographic meteors) predicts a similar result. This implies that slow meteors have vastly larger lags than fast meteors and, therefore, that their fragments should be much further spread along the trajectory. Such a spread, however, also implies some measurable spread across the trajectory, and a loss in radar echo strength that would be an extremely significant selection effect against radar observation of slow, fragmenting meteors. It would also be very difficult to recognize.

The working model described in Section 2.8 eliminates the original cause of worry about a selection effect; there is now no theoretical reason to expect that there should be a large class of meteors invisible to our radar. Practical demonstration that there is no such class is not possible by direct means. Nonetheless, we should expect a gradation from those meteors we can observe to those we cannot; the intermediate class of meteors would have shorter Fresnel patterns. Fortunately, we do not see any such intermediate class in appreciable numbers. The distribution of mean numbers of Fresnel extrema (MEXT) in Table 1 for slow meteors is bunched at high numbers; the tail toward low numbers is well explained by meteors close to the faint limiting magnitude of the system. Thus, we also have no practical reason to expect that many fragmenting meteors are lost.

2.11 Results

Several results from the fragmentation study thus far are important in their own right, and will also serve as the basis for quantitative studies of individual observed meteors. The spread (whole half-width) of the distribution of fragments along the trajectory averages 0.2 to 0.3 km. The centroid of ion production within that spread shifts significantly and systematically within the life of one meteor (but we have not deduced any systematic trend among meteors). The cause of the shift is probably inhomogeneous structure of the meteoroid. The result of the shift is very large errors in individual measures of deceleration.

The main body of most of our meteors does not ablate fragments layer by layer, but collapses rather suddenly under a dynamic pressure of the order of 2×10^4 dynes cm⁻². It is not yet certain whether this is quite independent of mass or velocity, or how much it varies among meteors. Evidently, this is the same class of meteors as those with sudden light-curve beginnings that formed 15% of McCrosky's (1955) Super-Schmidt meteors.

Our working model for these meteors envisages a gradation between two simple models. In case 1), the smallest (fastest) break up early in the observed trail and continue as a group of independent fragments. In case 2), the largest (slowest) are observed in the process of breaking up; the fragments have a relatively short independent existence.

The mean mass of meteoroid fragments is nearly independent of mass or velocity, and is of the order of 10^{-6} g.

Contrary to previous expectations from simplified theory, there is no reason to expect that many slow fragmenting meteors will be unobservable by radar. Moreover, we do not find any significant number that are marginally unobservable. We therefore do not think now that fragmentation causes a serious selection effect in our data.

3. DISTRIBUTION OF METEORS IN THE STREAMS DETECTED IN THE SYNOPTIC-YEAR SAMPLE

3.1 Introduction

The distribution of meteor orbits in the 256 streams of the synoptic-year sample (Southworth and Sekanina 1973) was studied in terms of the D-test, which measures the similarity of two orbits by the differences in their Keplerian elements (Southworth and Hawkins 1963). To express a stream's strength relative to the level of the sporadic background and the degree of dispersion of meteor orbits within the stream, the statistical model of meteor streams (Sekanina 1970) which is based on the D-test, defines two parameters of the D-distribution function of meteor orbits. The two parameters, the population coefficient Λ and the dispersion coefficient σ , also serve to determine the number of definite members of the stream in the sample used (Sekanina 1970), and to estimate the actual space density in meteor streams (Southworth and Sekanina 1973).

3.2 Determination of the Parameters Λ and σ

Until recently, the parameters Λ and σ of the D-distribution function were determined graphically (Sekanina 1970). This method required laborious plotting of the D-distribution curves. To avoid this, a new method has recently been developed.

The theoretical cumulative D-distribution, predicted by the statistical model, has the form:

$$N(D) = c \cdot f\left(\frac{D}{\sigma\sqrt{2}}\right), \qquad (23)$$

where N(D) is the number of meteors with the value of the D-test less or equal

to D, C is a constant of proportionality, and

$$f(E) = E^{3.8} + 2.64\Lambda \left[\int_0^E e^{-t^2} dt - Ee^{-E^2} \right]$$
 (24)

Since the parameters Λ and σ obviously cannot be determined explicitly, an iterative least-squares solution has been preferred, which starts from an arbitrary pair of values for Λ and σ in (23) and calculates differential corrections Δ log Λ and Δ log σ (as well as Δ log σ) from

$$\begin{vmatrix}
\Sigma \Delta \log N \\
\Sigma A_{\sigma} \Delta \log N
\end{vmatrix} = \begin{vmatrix}
n & \Sigma A_{\sigma} & \Sigma A_{\Lambda} \\
\Sigma A_{\sigma} & \Sigma A_{\sigma}^{2} & \Sigma A_{\sigma}^{A} \\
\Sigma A_{\Lambda} \Delta \log N
\end{vmatrix} \cdot \begin{vmatrix}
\Delta \log C \\
\Delta \log \sigma
\end{vmatrix}$$

$$\Delta \log A_{\Lambda} \Delta \log A_{\Lambda} = \Delta A_{\Lambda} = \Delta A_{\Lambda} \Delta \log A_{\Lambda} = \Delta A_{\Lambda}$$

where

$$A_{\sigma} = -\frac{3.8E^{3.8}}{f(E)} [1 + 1.389 \Lambda E^{-0.8} e^{-E^2}], \qquad (26)$$

$$A_{\Lambda} = \Lambda - \frac{E^{3.8}}{f(E)}$$

and

$$E = \frac{D}{\sigma\sqrt{2}}.$$
 (27)

3.3 Numerical results

Since the actual cumulative distribution of meteors in a stream is a byproduct of the main stream-search program, the above differential-correction
procedure can work directly with the punched output of the distribution data.

Practical calculations have shown that selection of arbitrary constants in the
place of the initial values of Λ and σ has created no problems and that in all
but six of the 256 cases the procedure converged successfully in less than 70
iterations and in most cases in less than 10 iterations. In four cases (May
Arietids, σ Draconids, L Cepheids and ε Umids) the method failed to converge,

and in two cases (April Ursids and ϵ Ursids) failed to yield any solution (the reason being that the slope of the D-curve at D < 0.1 was steeper than allowed by the model). In one other case (α Auriqids) the solution did converge, but indicated that this "stream" does not satisfactorily discriminate from the sporadic background.

Table 6 lists the results. An abbreviated name of the stream is given in the first column (an asterisk meaning that the stream was also detected in the 1961-65 sample) the parameters Λ and σ are in the second and third, respectively, the inner and outer limits, $D_{\rm I}$, $D_{\rm II}$, of the stream (for definition see Sekanina 1970) in the next two columns, and the number of definite members of the stream in the sample is in the last column. The definite members total 3182, or about 16% of the whole synoptic-year sample. A stream's population averages at about 12 to 13 meteors.

4. ON THE POTENTIAL ASSOCIATION OF FOUR METEOR STREAMS WITH THE MINOR PLANET ADONIS

4.1 The problem

There are four streams in the synoptic year sample with orbits similar to that of the minor planet Adonis: Capricornids-Sagittariids, Scorpiids-Sagittariids, χ Sagittariids and ϵ Aquarids. In terms of D the difference between the orbit of any of these streams and that of the minor planet is less than 0.2.

The orbital similarity may of course suggest the evolutionary relationship, implying that Adonis might have been a comet long time ago, and the meteor streams could be its debris. In that case the streams should indeed move in orbits similar to, but not identical with that of Adonis. The orbital difference is partly due to the non-zero momentum the ejected particles gained, enhanced by accumulation of differential perturbations by the planets since the time of ejection, partly due to the different size of the parent body and the debris.

4.2 The calculations

We have made an attempt to explore the observed difference between the orbits of Adonis and the orbits of the potentially associated streams to learn something on the time and circumstances of ejection.

Since Adonis has aphelion at 3.3 A.U. and close encounters with Jupiter are excluded, only secular perturbations were considered. Poynting-Robertson effect can be shown to accumulate over the spans of time considered here to not more than 0.09 A.U. in the semi-major axis, which is less than the uncertainty in the semi-major axis of the mean orbits of the streams. The effect of radiation pressure on the ejected particles was considered, although it appears to be less important than the other effects discussed below. For a zero ejection velocity the corrections to the five orbital elements due to radiation pressure are:

$$\Delta\omega_{rp} = -\frac{\sin v}{e} \frac{\Delta k^{2}}{k^{2}},$$

$$\Delta\Omega_{rp} = \Delta i_{rp} = 0,$$

$$\Delta q_{rp} = -q \frac{\Lambda - \cos v}{1 + e} \frac{\Delta k^{2}}{k^{2}},$$

$$\Delta e_{rp} = -(e + \cos v) \frac{\Delta k^{2}}{k^{2}},$$

$$(28)$$

where v is the true anomaly at the time of ejection, and $\Delta k^2/k^2 < 0$ is the relative reduction in the gravitational constant due to radiation pressure,

which amounts to

$$\frac{\Delta k^2}{k^2} = -\frac{6 \times 10^{-5}}{\rho_s a_s} Q_{rp} , \qquad (29)$$

 ho_s and a_s are the density and radius of the particle, $Q_{rp} \stackrel{:}{=} 1$ is the scattering efficiency for radiation pressure. The masses of meteoroids in the considered streams are about $10^{-4} g$, which gives typically $\rho_s a_s \stackrel{\sim}{=} 0.03 gm^{-2}$ and therefore $\Delta k^2/k^2 = -0.002$.

There are three other factors, determining the future orbit of an ejected meteoroid: the time of ejection, the position of the ejection point in orbit (involved also in the radiation-pressure effect (28)), and the ejection velocity (both magnitude and direction). If we know both the position of ejection in orbit, given by the true anomaly v, and the velocity of ejection, given by the radial $\dot{\xi}$ and transverse $\dot{\eta}$ components (ejection is assumed to be directed in the orbital plane), we can write for the corrections to the orbital elements of the parent body:

$$\Delta \omega = \frac{c}{e} \left[-\xi \cos v + \eta \frac{2 + e \cos v}{1 + e \cos v} \sin v \right],$$

$$\Delta\Omega = \Delta i = 0$$
,

$$\Delta q = -\frac{C_0 q}{1+e} \left[-\dot{\xi} \sin v + \dot{\eta} \frac{1 - \cos v + e \sin^2 v}{1 + e \cos v} \right], \quad (30)$$

$$\Delta e = C_0 \left[\xi \sin v + \eta \frac{2 \cos v + e(1 + \cos^2 v)}{1 + e \cos v} \right],$$

where

$$c_{o} = \frac{q^{1/2}(1+e)^{1/2}}{v} \tag{31}$$

and $v = 2.978 \times 10^4$, if $\dot{\xi}$ and $\dot{\eta}$ are expressed in meters per second.

The model calculations started with running the orbit of Adonis back for 12000 years, applying the secular perturbations by Jupiter to Neptune. Based on our previous experience (Sekanina 1971), we assumed ejections to take place at five discrete times 4000 to 12000 years ago, always 2000 years apart. each time, ejections were considered to take place at 1.2 A.U. and 0.7 AU from the sun before perihelion, at perihelion, and also 0.7 and 1.2 A.U. after perihelion. The ejections were then assumed to be directed toward the sun and also deviating by 30° and by 60° both in and opposite to the direction of motion. Finally, the magnitude of the ejection velocity was estimated from Probstein's (1968) fluid-dynamics model. Assuming that at the time of ejection the radius of Adonis was between 1 and 20 km, the vaporization rate between 1 \times 10¹⁷ and 7 \times 10¹⁷ molecules/cm² sec and surface temperature 190° to 200° K (both fitting a range of values for water snow), the minimum ejection velocity, $v_e = (\dot{\xi}^2 + \dot{\eta}^2)^{1/2}$, of meteoroids of $\rho_s a_s = 0.03$ g cm⁻² would vary as 17/r $(m \sec^{-1})$, the maximum velocity as 200/r $(m \sec^{-1})$, where r is the heliocentric distance in A.U. A case with 60/r (m sec-1) was also considered, assumed to be a reasonable mean value.

4.3 The results

Altogether, therefore, five ejection times were considered with 5 x 5 x 3 = 75 options in each case, or a total of 375 individual models. For each of them the initial orbital elements were computed from the orbital elements of Adonis at the time of ejection, adding the corrections due to radiation pressure

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Table 1. Data from 3550 Synoptic Year meteors.

DECEL.	.32-1.0	1.6-3.2	3.2-10.	1032-	32100.	100.466	ALL DECEL.
LOGIO PASS	CVER -2	OVER -2	CVEF -2	OVER -2	OVER -2	GVER -2	OVER -2
C(/010 17733	CVEN -2	OVEN -2	016, -2	OVEN -Z	OVER -E	OTER -E	0454 -5
FRACT	·6197	.0620	.0315	.0025	0.0000	0.000	.1163
A VILAR	16.2774	17.6926	18.6872				17.6397
AV DECEL	.6831	1.9578	4.7830		* •		2.7722
TX31 VA	20.7714	20.3046	19,1072				14.9734
AV L FROM	-1.6002	-2.7070	-3.7759				-2.8434
AV L FRC N	.4277	1.3167	2.1724		٠,		1.4292
					. *		664
, ⁴EXT5 - 7	0.000	.0045	.0089		•		-004b
8-12	.1256	.1273	.1429				.1404
13-19	3857	.3091	.3929				.3414
20-30	•4857	.5591	4554				.5133
L FFG MASS	• 9429	.8500	.5536		•	• •	.7724
-4 TC -5	.0143	.1000	.2321				.1211
-5 TO -6	0286	0318	1518			•	.0678
-6 TO -7	.0143	.0136	.0357				.0266
LE -7	0.0000	.0045			•		.0121
·	04000		*	•			
L FRG NUMB	.4714	.1545	.0536				.1840
0 TG 2	.3857	.5455	.4107				.4697
. 2 TG 4	1286	.2727	.4196				.2833
4 TC 6	0.0000	.0227	.1071				.0533
GE 6	.0143	.0045	.0089		•	•	.0097
		1200	87.1616			•	67.1823
HMAX	87.7200	87.1200					12.0930
TRAIL LEN.	11.7609	12.4825	11.6621				3.7700
MMAX-ML IF	3.6700		3.8723				11.3360
MAGN (MAX)	11.4986	•	11.2321				-10.9034
LOG SIGMA	-10.3914	-10.8744	-11.2345				-10.9034
DECEL.	-	1.0-3.2	3,2-10,	10 _e =3 <u>2</u> ,	32100.		ALL DECEL.
DECEL. LOGIO'MASS	-		3.2-10. -2 TO -3			100,+UF -2 TO -3	ALL DECEL. -2 TO -3
LOGIO'MASS	-2 TO -3	-2 TO -3	-2 TO -3	-2 10 -3	-2 TO -3	-2 TO -3	.=2 10 =3
LOGIO MASS	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3			.=2 TO =3 •2975
FRACT AV VMAX	-2 TO -3 .0093 24.0291	-2 TO -3 .0842 24.9598	-2 TO -3 .1724 26.0872	-2 10 -3 .0293 28.0422	-2 TO -3	-2 TO -3	-2 TO -3 -2975 25,9091
FRACT AV VMAX AV DECEL	-2 TO -3 .0093 24.0291 .7170	-2 TO -3 .0842 24.9598 2.1965	-2 TO -3 .1724 26.0872 5.5707	-2 TO -3 .0293 28.0422 13.5287	-2 TO -3	-2 TO -3	.=2 TO =3 .2975 25.9091 5.6622
FRACT AV VMAX AV DECEL AV MEXT	-2 TO -3 .0093 24.0291 .7170 21.1212	-2 TO -3 .0842 24.9598 2.1965 20.0301	-2 TO -3 .1724 26.0872 5.5707 19.0147	-2 TO -3 .0293 28.0422 13.5287 17.1058	-2 TO -3	-2 TO -3	.=2 TO =3 .2975 25.9091 5.6622 19.1278
FRACT AV VMAX AV DECEL	-2 TO -3 .0093 24.0291 .7170	-2 TO -3 .0842 24.9598 2.1965	-2 TO -3 .1724 26.0872 5.5707 19.0147 -4.0321	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283	-2 TO -3	-2 TO -3	.=2 TO =3 .2975 25.9091 5.6622 19.1278 -3.7311
FRACT AV VMAX AV DECEL AV MEXT	-2 TO -3 .0093 24.0291 .7170 21.1212	-2 TO -3 .0842 24.9598 2.1965 20.0301	-2 TO -3 .1724 26.0872 5.5707 19.0147	-2 TO -3 .0293 28.0422 13.5287 17.1058	-2 TO -3	-2 TO -3	.=2 TO =3 .2975 25.9091 5.6622 19.1278
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800	-2 TO -3 .1724 26.0872 5.5707 19.0147 -4.0321 1.4260	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022	-2 TO -3	-2 TO -3	.=2 TO =3 .2975 25.9091 5.6622 19.1278 -3.7311
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800	-2 TO -3 .1724 26.0872 5.5707 19.0147 -4.0321 1.4260 .0098	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022	-2 TO -3	-2 TO -3	2 TO -3 .2975 25.9091 5.6622 19.1278 -3.7311 1.1522
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003	-2 TO -3 .1724. 26.0872 5.5707 19.0147 -4.0321 1.4260 .0098 .1225	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .5000	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003	-2 TO -3 .1724. 26.0872 5.5707 19.0147 -4.0321 1.4260 .0098 .1225	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .5000 .3365	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .5000 .3365	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364 .9697 0.0000 0.0000	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .5000 .3365	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .5000 .3365	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364 .9497 0.0000 0.0000 0.0000 0.0000	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MA5S -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364 .9697 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .5000 .3365 .3173 .2308 .0865 .0481	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364 .9697 0.0000 0.0000 0.0000 .0303 0.0000 .8485 .1212	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100	-2 TO -3	-2 TO -3 .0293 28.0422 13.5287 17.1058 -4.6283 1.9022 .0385 .1250 .3173 .3173 .2308 .0865 .0481	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364 .9697 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2	-2 TO -3	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4	-2 TO -3 .0093 24.0291 .7170 21.1212 -1.3778 -1.0124 0.0000 .0909 .2727 .6364 .9697 0.0000 0.0000 .0303 0.0000 .8485 .1212 0.0000	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4 4 TO 6 GE 6	-2 TO -3	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100 .3478 .5753 .0635 .0100 .0033	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4 4 TO 6 GE 6 HMAX	-2 TO -3	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100 .3478 .5753 .0635 .0100 .0033	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4 4 TO 6 GE 6 HMAX TRAIL LEN.	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT S-7 8-12 13-19 20-30 L FRG MASS -4 TO -6 -5 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4 4 TO 6 GE 6 HMAX LEN. MMAX-MLIM	-2 TO -3	-2 TO -3 .0842 24.9598 2.1965 20.0301 -2.9748 .4800 .0067 .1003 .3746 .5184 .8595 .0803 .0468 .0033 .0100 .3478 .5753 .0635 .0100 .0033	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB 0 TO 2 2 TO 4 4 TO 6 GE 6 HMAX TRAIL LEN.	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3	-2 TO -3

Table 1. (Cont.)

	42-1 ft	1.0-3.2	3.2-16.	1032.	32100.	100.+UF	ALL DECEL.
DF CFr.							
LCG10 MASS	-3 10 -4	-3 TO -4	-3 10 -4	-3 10 -4	-3 TO -4	-3 TU -4	-3 TU -4
EGACT	•0023	.0321	.1904	.1496	.0034	0.0000	•3777
AV VIAX	33.1425	31,7109	32,7491	34.7395	35.0267		33.4717
AV CECEL	-B012	2.2738	6.7020	14,9699	48.8558		9.9414
AV LLCEL	17.2500	16.3070	15.6805	14.5085	11.5000	•	15.2416
	-1.7453	-3.2648	-4.4007	-5.2542	-7.0461		-4.6516
AV L FRG M		0486	9779	1.7148	3.3768		1.1885
AV L EKG N	-1.5956	0460			343,42		* * * *
	0.0000	00.0	0147	.0132	.0833		.0149
≛FλT 5=7	0.0000	.00bB	.0163	.2881	.4167		.2269
8-12	.1250	.1491	.1938	•	.3333		.6003
13-19	.7500	.6404	-6124	.5800			.1559
20-30	.1250	.2018	.1775	,1186	.1667		•
			***		0.0000		.2804
L FRG MASS	1.0000	.7719	.3107	.1318			.3415
-4 TO -5	0.0000	.1491	4201	.2957	0.0000		2453
-5 TC -6	0.0000	.0702	.2012	.3427	2500		0820
-6 TO -7	0.0000	. . u088	.0503	.1318	4167		-
LE -7	0.0000	(· , 0000	.0178	.0979	.3333		.0507
							1500
L FRG HUMB	1.0000	.4649	.1627	.0791	0.0000		.1588
U TO 2	0.0000	.5000	.6864	.5556	.6833		6092
2 TO 4	0.0000	.0351	.1435	.3164	.6667		.2066
4 TU 6	0.0000	0.0000	.0044	.0377	.1667		.0186
GE 6	0.0000	0.0000	.0030	.0113	.0833		•0067
3. 0	. • • • • •	-					
HMAX	93.0375	92.9000	92.4734	92.3034	93.7167		92.4568
TRAIL LEN.	12.7221	12.0105	11.9524	11.3054	10.0895		11.6891
MMAX-MLIN	3.6500	3.4061	3.4731	3.7228	3.5250		3.5678
MAGN (MAX)	11.2125	11.4974	11.4558	11.2089	11.3917	•	11.3595
	-10.5162	-16.9312	-11.3934	-11.7205	-12.1758		-11.4854
LOG SIGMA	-1043106						
NECEL	22 1 0	1 0-3 3	3 7-10-	1032.	32.=100.	LOO. +UP	ALL DECEL.
DECEL.		1.0-3.2			32.=190.		
DECEL. LOGIO MASS					37190. -4 TO -5		ALL DECEL. -4 TO -5
	-4 TO +5	-4 TO -5	-4 TC -5	-4 TO -5	-4 TO -5	-4 TO -5	-4 TO -5
			-4 TC -5	-4 TO -5	-4 TO -5		-4 TO -5
LOGIO MASS	-4 TO +5	-4 TO -5	-4 TC -5	-4 TO -5 .0879 44.7239	-4 TO -5 .0220 49.8241	-4 TO -5	-4 TO -5 .1439 45.0827
LOGIO MASS	-4 TO +5	-4 TO -5	-4 TC -5 .0313 43.1657 7.0659	-4 TO -5 .0879 44.7239 17.8241	-4 TO -5 .0220 49,8241 48,4267	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588
FRACT AV VMAX	-4 TO +5	-4 TO -5 .0028 46.5710	-4 TC -5 .0313 43.1657	-4 TO -5 .0879 44.7239	-4 TO -5 .0220 49.8241	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190
FRACT AV VMAX AV DECEL	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140	-4 TC -5 .0313 43.1657 7.0659	-4 TO -5 .0879 44.7239 17.8241	-4 TO -5 .0220 49,8241 48,4267	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446
FRACT AV VMAX AV DECEL AV MEXT	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000	.0313 43.1657 7.0659 12.1802	-4 TO -5 .0879 44.7239 17.8241 11.3269	-4 TO -5 .0220 49.8241 48.4267 9.8077	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M	-4 TO +5	-4 TO -5 .0028 46.5710 2.5140 13.3000 -3.1816	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M	-4 TO +5	-4 TO -5 .0028 46.5710 2.5140 13.3000 -3.1816	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687	-4 TO -5 ,0220 49,8241 48,4267 9,8077 -6,4697 1,8294	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000 .9000 1000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483
LOGIO MASS FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000 .1000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .0641 .0385 .1795 .4359	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000 .9000 1000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000 .1000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000 .9000 0.0000 0.0000 0.0000 0.0000	-4 TC -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .5000 .2000 .9000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821 .1026 .4359	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035
LOGIO MASS FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .5000 .2000 .7000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .3974	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605
LOGIO MASS FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .2000 -7000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603 .0096	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .3974 .0385	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605 .0117
LOGIO MASS FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .5000 .2000 .7000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .3974	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605
LOGIO MASS FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .5000 .2000 .7000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000 0.0000	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603 .0096 .0032	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .3974 .0385 .0256	-4 TO -5	-4 TO -5
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG M MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6 HMAX	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .5000 .2000 .7000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000 0.0000 94.1775	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603 .0096 .0032	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .3974 .0385 .0256	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605 .0117 .0059
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG M MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 T0 -5 -5 T0 -6 -6 T0 -7 LE -7 L FRG NUMB 0 T0 2 2 T0 4 4 T0 6 GE 6 HMAX TRAIL LEN.	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .5000 .2000 1000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000 0.0000 94.1775 10.7623	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603 .0096 .0032	-4 TO -5 ,0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .2051 .0769 .0641 .0385 .1795 .4359 .2821 .1026 .3974 .0385 .0256	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605 .0117 .0059 94.1207 10.1793
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6 HMAX TRAIL LEN. MMAX-MLIM	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .2000 .9000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000 0.0000 94.1775 10.7623 3.3378	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603 .0096 .0032	-4 TO -5 ,0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .2821 .1026 .3974 .0385 .0256	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605 .0117 .0059
LOGIO MASS FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6 HMAX TRAIL LEN MAGN (MAX)	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .2000 .2000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000 0.0000 94.1775 10.7623 3.3378 11.4712	-4 TO -5	-4 TO -5 .0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .3974 .0385 .0256	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3146 .5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3483 .1957 .0861 .2035 .6184 .1605 .0117 .0059 94.1207 10.1793 3.5804 11.2481
FRACT AV VMAX AV DECEL AV MEXT AV L FRG M AV L FRG N MEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6 HMAX TRAIL LEN. MMAX-MLIM	-4 TO +5	-4 TO -5 .0028 40.5710 2.5140 13.3000 -3.1816 -1.1146 0.0000 .3000 .2000 .9000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	-4 TU -5 .0313 43.1657 7.0659 12.1802 -4.3703 .0161 .0270 .5495 .3694 .0541 .2613 .5135 .2162 0.0000 .0090 .4324 .5586 .0090 0.0000 0.0000 94.1775 10.7623 3.3378	-4 TO -5 .0879 44.7239 17.8241 11.3269 -5.4793 1.0687 .0417 .5705 .3333 .0545 .0673 .2051 .4487 .2115 .0673 .1218 .7051 .1603 .0096 .0032	-4 TO -5 ,0220 49.8241 48.4267 9.8077 -6.4697 1.8294 .1410 .5769 .0641 .0385 .1795 .4359 .2821 .1026 .4359 .2821 .1026 .3974 .0385 .0256	-4 TO -5	-4 TO -5 .1439 45.0827 19.8588 11.3190 -5.3446 .9135 .0528 .5616 .3249 .0607 .1252 .2446 .3497 .0861 .2035 .6184 .1605 .0117 .0059 94.1207 10.1793 3.5804

Table 1. (Cont.)

							•
D=C=1	33-1-0	1.0-3.2	3.2-10.	1032.	32100.	100.+UP	ALL DECEL.
DECEL.	.32-1.0						
LOGIO MASS	~5.LOWER	-5.LOWER	-5.LOWER	-5.LOWER	-5.LOWER	-5.LOWER	-5.LOWER
			0051	0230	.0318	.0037	.0645
FRACT	0.0000	0.0000	.0051	.0239			57.4659
AV VMAX			55.2972	56.4162	58,2167	60.8046 145.2369	42.1600
AV DECEL			7.4933	19,6926	52.7240		8.7162
AV MEXT			9.2778	B.9177	8.4956	8.5385	_
AV L FRG M.			-4.6235	-5.6636	-6.5798	-7.7659	-6,1533
AV L FRG N.	•		6193	.3398	1.1366	2.1653	.7612
4					1770	.3077	.1703
MEXT 5-7			.0556	.1647	•1770	.3846	5983
8-12			.9444	.6824	.5044 .2212	.3077	.1485
13-19			- 0.0000	.0588	0973	0.0000	.0830
20-30		· .	0.0000	.0941	107/3	040000	*0430
			.0556	.0471	.0265	0.0000	.0349
L FRG_MASS			7778	1176	.0708	.0769	.1441
-4 TU -5			.1667	4706	.1062	0.0000	2402
-5 TG -6			0.0000	3529	.3982	.1538	.3362
-6 TU -7			0.0000	.0118	.3982	.7692	2445
LE -7			0,0000	•0110		•	·
t FEG BULL			.9444	.2824	.1150	.0769	.2402
6 TC 2			0556	.7059	.7345	.2308	+6419
2 TC 4			0.0000	0118	.1504	.6154	.1135
4 70 6			0.0000	0.0000	0.0000	.0769	.0044
GE 6			0.0000	0.0000	0.0006	0.0000	0.0000
42 0							05 / 7//
HHAX	-		96,5611	96.1400	94,9230	94.4538	95.4769
TRAIL LED.			9,8857	9.4502	8.0671	7.5814	8,6958
HHAX-MLIN			3,2167	3.2847	3.3956	3.2308	3.3310
HAGE (MAX)			11.5000	11,4918	11.3726	11.3769	11.4271
LOG SIGNA			-11,3711	-11,7621	-12.1183	-12.5462	-11.9517
DECEL	.32+1.0	1.0-3.2	3.2-10.	1032.	32100.	100.+UP	ALL DECEL.
		ALL MASS	ALL MASS			ALL MASS	ALL MASS
LOGIO MASS	ALL MASS	ALL MASS	VEC LIMBS	ALL MASS	HEE WASS	MEE WHOS	,,
f :	. 317	.1011	.4307	.2932	.0592	.0037	1.0000
FRACT	.0313 19.7975	23.9131	30.0888	38.7154	52.7705	60.8046	32,6226
AV PLOEI	7017	2.1334	6.1443	16.0626	51.4463	145,2369	11.3403
AV DECEL	20.6216	19.3593	16.9366		9.2000	6.5385	
AV NEXT AV L FRG M				13-3040		04////	15,9625
AV L FRG N		_2.9414		13,3698 -5,2907		-7.7659	15.9645 -4.3646
		-2.9414 -6478	-4.2078	-5.2907	-6.6132 1.6665	-	•
HA F LUC. II		-2.9414 -6478			-6,6132	-7.7659	-4.3640 1.1386
_	1463	.6478	-4.2078 1.1561	-5.2907	-6,6132	-7.7659	-4.3640 1.1386 .0287
►EXT 5=7	1463 0.0000	.6478	-4.2078	-5.2907 1.4425	-6.6132 1.6665	-7.7659 2.1653	-4.3640 1.1386 .0287 .2566
ՒĒXT 5=7 8=12	1463 0.0000 .1171	.6478 .0062 .1213	-4.2078 1.1561 .0144	-5.2907 1.4425 .0365	-6.6132 1.6665 .1619	-7.7659 2.1653 .3077	-4.3640 1.1386 .0287 .2566 .4431
►EXT 5-7 8-12 13-19	1463 0-0000 -1171 -3784	.6478 .0062 .1213 .4012	-4.2078 1.1561 .0144 .1962	-5.2907 1.4425 .0365 .3900	-6.6132 1.6665 .1619 .5143	-7.7659 2.1653 .3077 .3846	-4.3640 1.1386 .0287 .2566
ՒĒXT 5=7 8=12	1463 0-0000 -1171 -3784	.6478 .0062 .1213	-4.2078 1.1561 .0144 .1962 .4899 .2995	-5.2907 1.4425 .0365 .3900 .4524 .1210	-6.6132 1.6665 .1619 .5143 .2333 .0905	-7.7659 2.1653 .3077 .3846 .3077 0.0000	-4.3640 1.1386 .0287 .2566 .4431 .2715
►EXT 5-7 8-12 13-19	1463 0.0000 .1171 .3784 .5045	.6478 .0062 .1213 .4012 .4712	-4.2078 1.1561 .0144 .1962 .4899 .2995	-5.2907 1.4425 .0365 .3900 .4524 .1210	-6.6132 1.6665 .1619 .5143 .2333 .0905	-7.7659 2.1653 .3077 .3846 .3077 0.0000	-4.3640 1.1386 .0287 .2566 .4431 .2715
NEXT 5-7 8-12 13-19 20-30	1463 0.0000 .1171 .3784 .5045	.6478 .0062 .1213 .4012 .4712	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000	-4.3640 1.1386 .0287 .2566 .4431 .2715
NEXT 5-7 8-12 13-19 20-30 L FRG MASS	1463 0.0000 .1171 .3784 .5045 .9550	.6478 .0062 .1213 .4012 .4712 .8414 .0995	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 .0769 0.0000	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4: TO -5	1463 0.0000 -1171 -3784 -5045 -9550 -0090 -0180	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 0.0000 .0769 0.0000 .1538	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4: TO -5 -5 TO -6	1463 0.0000 .1171 .3784 .5045 .9550 .0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 .0769 0.0000	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011
FRG MASS -4: TO -5 -5 TO -6 -6 TO -7 LE -7	1463 0.0000 .1171 .3784 .5045 .9550 .0090 .0180 0.0000	.6478 .0062 .1213 .4012 .4712 .8414 .0945 .0451 .0062	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4: TO -5 -5 TO -6 -6 TO -7 LE -7	1463 0.0000 -1171 -3784 -5045 -9550 -0090 -0180 0.0000	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 0.0000 .0769 0.0000 .1538	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4: TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2	1463 0.0000 .1171 .3784 .5045 .9550 .0090 .0180 0.0000	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692 .0769 .2308	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3936 .2572 .2011 .0930 .0558
FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4	1463 0.0000 .1171 .3784 .5045 .9550 .0090 .0180 0.0000 .6216 .2793 .0811	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692	-4.3640 1.1386 .0287 .2566 .4431 .2715 .393C .2572 .2011 .093U .0558
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4: TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6	1463 0.0000 -1171 -3784 -5045 -9550 -0090 -0180 0.0000 -6216 -2793 -0811 -0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062 .3126 .5428 .1291 .0124	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507 .0307	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 0.0769 0.0000 .1538 .7692 .0769 .2308 .6154	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558
FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4	1463 0.0000 .1171 .3784 .5045 .9550 .0090 .0180 0.0000 .6216 .2793 .0811	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170 .0052	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619 .1000 .5619 .2714 .0381 .0286	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692 .0769 .2308 .6154 .0769 0.0000	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558 .1851 .5845 .2017 .0214
FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6	1463 0.0000 .1171 .3784 .5045 .9550 .0090 .0180 0.0000 .6216 .2793 .0811 .0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062 .3126 .5428 .1291 .0124 .0031	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507 .0307 .0307 .0308	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619 .1000 .5619 .2714 .0381 .0286	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692 .0769 .2308 .6154 .0769 0.0000 94.4538	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558 .1651 .5845 .2017 .0214 .0073
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6	1463 0.0000 -1171 -3784 -5045 -9550 -0090 -0180 0.080 0.080 -6216 -2793 -0811 -0090 -0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062 .3126 .5428 .1291 .0124 .0031	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170 .0052	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507 .0307 .0086	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619 .1000 .5619 .2714 .0381 .0286 94.3848 8.5176	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 0.769 0.0000 .1538 .7692 .0769 0.2308 .6154 .0769 0.0000 94.4538 7.5814	-4.3640 1.1386 .0287 .2566 .4431 .2715 .393C .2572 .2011 .093C .0558 .1851 .5845 .2017 .0214 .0073
PEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6	1463 0.0000 -1171 -3784 -5045 -9550 -0090 -0180 0.080 0.080 -6216 -2793 -0811 -0090 -0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062 .3126 .5428 .1291 .0124 .0031	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170 .0052	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507 .0307 .0086 92.7248 10.8745 3.6949	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619 .1000 .5619 .2714 .0381 .0286 94.3848 8.5176 3.6429	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692 .0769 .2308 .6154 .0769 0.0000 94.4538 7.5814 3.2308	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558 .1851 .5845 .2017 .0214 .0073
NEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6 HMAX TRAIL LEN.	1463 0.0000 -1171 -3784 -5045 -9550 -0090 -0180 0.0000 -6216 -2793 -0811 -0090 -0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062 .3126 .5428 .1291 .0124 .0031	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170 .0052 91.3329 12.3249 3.5701 11.3917	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507 .0307 .0086 92.7248 10.8745 3.6949 11.2115	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619 .1000 .5619 .2714 .0381 .0286 94.3848 8.5176 3.6429 11.1248	-7.7659 2.1653 .3077 .3846 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692 .0769 .2308 .6154 .0769 0.0000 94.4538 7.5814 3.2308 11.3769	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558 .1851 .5845 .2017 .0214 .0073 91.5656 11.6913 3.6202 11.3276
PEXT 5-7 8-12 13-19 20-30 L FRG MASS -4 TO -5 -5 TO -6 -6 TO -7 LE -7 L FRG NUMB O TO 2 2 TO 4 4 TO 6 GE 6	1463 0.0000 -1171 -3764 -5045 -9550 -0090 -0180 0.0000 -6216 -2793 -0811 -0090	.6478 .0062 .1213 .4012 .4712 .8414 .0995 .0451 .0078 .0062 .3126 .5428 .1291 .0124 .0031 .49.8042 .12.5887 .3.6126 .11.4117	-4.2078 1.1561 .0144 .1962 .4899 .2995 .3970 .3734 .1733 .0379 .0183 .1629 .6200 .1949 .0170 .0052	-5.2907 1.4425 .0365 .3900 .4524 .1210 .1249 .2546 .3727 .1710 .0768 .1085 .6013 .2507 .0307 .0086 92.7248 10.8745 3.6949 11.2115	-6.6132 1.6665 .1619 .5143 .2333 .0905 .0381 .0524 .1429 .4048 .3619 .1000 .5619 .2714 .0381 .0286 94.3848 8.5176 3.6429	-7.7659 2.1653 .3077 .3646 .3077 0.0000 0.0000 .0769 0.0000 .1538 .7692 .0769 .2308 .6154 .0769 0.0000 94.4538 7.5814 3.2308	-4.3640 1.1386 .0287 .2566 .4431 .2715 .3930 .2572 .2011 .0930 .0558 .1851 .5845 .2017 .0214 .0073

Table 2. Additional data for the mass groups of Table 1.

log ₁₀ mass range (g)	> -2	-2 to -3	-3 to -4	-4 to -5	< - 5
Limit to number of extrema at mean range and velocity	123	61	37	21	13
Mean observed extrema	20.0	19.1	15.2	11.3	8.7
Loewenthal's C at mean height and velocity	0.039	0.043	0.050	0.047	0.046
Width of last two observed Fresnel zones (km), a high approximation to fragment spread	0.18	0.19	0.22	0.26	0.31

30

Table 3. Computed lag and width of last two Fresnel zones (km).

· · · · · · · · · · · · · · · · · · ·	. <u> </u>	<u> </u>				·	
	Decel:	0.32-1.0	1.0-3.2	3.2-10	10-32	32-100	100 + up
log m >-2	L _{max}	0.02	0.06	0.12			
	$^{ m L}$ end	0.14	0.39	0.75			
÷	ή-	0.18	0.18	0.18			,
-2 to -3	L	0.01	0.04	0.09	0.16		•
	Lend	0.08	0.20	0.57	0.92		
	M.	0.18	0.18	0.19	0.20		
-3 to -4	L _{max}		0.02	0.06	0.11	0.30	
	Lend		0.15	0.36	0.64	1.67	
	W		0.22	0.22	0.24	0.25	
-1 to -5	Lmax		0.01	0.03	0.07	0.12	
	L _{end} .	·	0.06	0.18	0.39	0.64	
	w		0.23	0.24	0.25	0.27	
≤-5	L max			0.02	0.04	0.09	0.19
	L _{end}			0.10	0.23	0.49	0.95
	w. end			0.28	0.28	0.29	0.29

Table 4. Mean vertical trail lengths.

<u> </u>	h _{beg} -h _{end} (km)							
M _{lim} -M _{max}	Simple theory	Short trail	Synoptic year ^o l					
0	0.0	7.8	(7.3 ± 2.4)					
. 2	19.0	10.4	7.4 ± 2.5					
. 4	29.8	18.9	(8.3 ± 2.8)					
6	40.0		,					

Table 5. Mean vertical trail lengths and radiant zenith distance.

cos Z _R	Mean cos Z _R	h _{beg} -h _{end}	σ ₁
0 to 0.2	0.143	1.71	0.59
0.2 to 0.4	0.318	3.81	1.04
0.4 to 0.6	0.514	6.14	1.90
0.6 to 0.8	0.715	8.07	2.44
0.8 to 1	0.847	8.38	2.53

	8		NS.	STREAM	LAMBDA	SIGNA	DI	DII	NS	STREAM	LAMBDA	SIGHA	DI	DII	NS
STREAM LANGDA	SIGNA D	01 011				.042	.104	.171	7	B CAMELOP	14	.047	.107	.166	9
		18 .167		MU 5AGIT AQUA-AGUIL	24 190	.020	.063	-141	5	H CAMELOP ALP CAMEL	18 8.6	.060 .058	.142	.227 .160	11
		25 •203 192 •331	11	CHI SAGITT	8800 00	.010 .035		.193 .202	6	SEPT URSID	90	.048	+140	.277	4-
TH COR BOR 26	.047 .1	118 -196		P DRACONID BOOT-DRACO	90 6800	.009	.037	162	2	DRACO-UMID	13 15	.057 .055	.128 .127	.198 .198	13
LAM BOOTID \$60)62 .161 141 .221		J DRACONID	23	.053	.130	.214	7	META DRACO	5.0	.083	.154	.220	10
CORONA BUR 21 CANIDS 270	.031 .1	101 .23	y 5	EPS CEPH Beta andr	46 640	.047	066	.228 .184	ż	SEPT DRACO	6.6 4.7	.053	.105 .137	.152 .195	8 25
#GUAUKART 16		128 .201 084 .21		LACERTID	22	.064	. 156	.255	12 65	APISCIDS SEPT CEPH	2.0	.132	.188	256	31
JAN SAGIT 420 JAN URACO 77	.032 .0	092 .17	8 9	OMEGA DRA CYGN-DRACO	5.8 18	.147	.282 .206	.407 .329	18	ARIET-PISC	14	.060	.136	.212	16 5
#DEL CANCE 5.2		135 .19: 159 .22:		KAPPA PER	250	.025	.081	.189	5 .	#GAPMA PIS Gampa arie	140	.032	.098	205	6
JAN CANCR 5.5 PSI LEGGID 11		146 .22	•	KAPPA AUR	20 28	.042 .037	.101 .094	.163 .157	3 6	ETA PERS	86	.037	.107	-211	6 5
XI SAGIT 4.B	.106	195 .27		#BETA TAUR	15	077	.177	.277	24	X1 CEPHEID RHC PISCID	45 170	.034	.091 .084	.164	6
JAN AGUAR 53 #CAPR-SAG 11		164 .19 164 .24	-	YPS DRACU	120	.032	.096	.199	10	KAPPA CEPH	40	.040	.106	.187	12
H DRACONID 96	.029	085 .17		SIGMA CASS	17 75	,059 .033	054	.182	6	F CEPHEID SEPT CASS	57 20	.036	.100 .125	.184 .202	9
IODTA DRA 28 PS1 CYGNID 260	.053	134 .22 100 .23	- :	JULY CASS	52	.034	.093	.170 .209	6 7	D CASSIOP	580	.022	.076	.208	4
MALPHA LEG 4.9	.085 .	162 .23	2 12	RHO DRACO Kappa Cass	51 35	.042	.115	.19B	6	H CEPHEID	120	.067 .029	.148 .087	.227 .181	8
LAM CAPR 37 ADELTA LEG 5.2		157 .27 257 .36		CASSIOPEID	13	.066	148	.229	17 5	GAFFA UMID D LRSID	20	.046	.111	.179	5
EPS ADDAR 644	.109	214 .31	1 20	#JUL DHACO	420 29	.022	.074	.266	ý	SEPT CAMEL	32	.040 .068	.103 .136	.176	11 17
FEB DRACG 4.1		178 .25 109 .21		ZETA URSID	9.7	.061	130	.195	13 11	CAMELOPARD SEPT UMID	7.1	.059	.133	.205	9
XI CYGNID 99 KAPPA GEM 110	.023	068 14	iÒ 4	PSI CASS	23 7.3	.059	.145	.23B .269	17	A CAMELOP	660	.013	.045	.127 .375	8 32
RHO LEDNID 12		104 .15		CANES VEH OHI DRACO	57	.037	.102	190	4	D CRACONIC		.116	.163	224	23
MU LEONID 28 #P1 VIRGIN 13		101 -17 130 -20	18	PJ AGUARID	9.3	.093 .041	.197 .118	.294 .230	21 37	DCT ANDROP	32	.043	111	.189 .198	7 10
aN ETA VIR 14	.064	146 .22		AS DEL AQU A CEPHEID	- 81 18	071	.168	. 268	20	OCT CEPH G CEPHEID	8.1 380	.065	.134	169	5
LEO-URSID 110 as eta vir 37		.092 .18 .134 .23	· ·	CEPH-DHACO		.054	139 109	.23B	9 10	HOCT DRACE	21	.055	.133	.217	18 7
MAR HERCUL 440	.026	U68 .27		OMI CEPH 10DTA CEPH	24 28	034	.086	.145	5	K CAMELOP THET DRACE	56 3.1	.045	124	.230	25
CHI HERCUL 980		.065 .19 .116 .15		B CASSIOP	51	.040	.109	.199	7 10	SEXTANTID	240	.037	.119	.277	5
#5 VIRGIN 2.2 MAR VIRGIN 8.2	060	124 .10	83 5	GAMMA CEPH B CEPHEID	5.3 110	.067 .027	.126	165	6	L CAMELOP	38 90	.041	.108 .137	.189 .272	7
MAR LYRID 55 HERCUL-LYR 200		.121 .2: .073 .10		TODTA CASS	13	.061	.137	.211 .156	9 8	DEL URSID J CAMELOP	460	.023	.078	.204	6
HERCUL-LYR 200	.012	043 -1	30 4	MU CANCRID D CAMELOP	140 930	.024	.073 .050	150	6	HLAM DRACE	10 8.3	.094 .118	202 244	.303 .362	20 33
api DRACO 17		.117 .14 .116 .14		E DRACONIC	18	.059	.140	.223 .219	13	A URSID N GRACONII		.031	.086	.159	4
#N VIRGIN 6.0 #LIBRIDS 86	.025	.073 .1	43 4	L DRACONIO			.107 .129	196	ii	G CAMELOP	19	.045	.108	.173	6 29
LAM AURIG 12		140 .2		*AGJ_CAPR	16	.076	.177	.279	22 23	DRACD-CAM C URSID	7.8 20	.075	.132	.214	9
#APR VIRG 49 NU HERCUL 120	.035	.105 .2	18 7	#ALPHA CAF			*0R5	237 149	10	+5 ARIETI		.128	.266 168	395 255	99 8
MALPHA VIR 23		.093 .1 .135 .2		MBETA CEP	" 97	.032	.094	.189	6	PSI VIRGIONIDS	N 11 76	.077	.126	.243	8
EPS LYRID 79 APR CYGNID 15		.198 .3	10 16	C DRACONII	8.9 21		.193	.288 .209	26 16	M CEPHEID	44	.041	.110	.196	5 3
MMAR ANDR 6-1	.084	.163 .2 .138 .2	36 12 37 7	AUG CASS GAMMA CYGI		.032	.094	.189	5	E CEPHEID BETA CAME	330 L 190	.019	088	197	4
D DHACCNID 34 GAMMA VIRG 190		091 .2	04 4	PERSEIDS	470 5 2400		.088	.232 .178	3	8 URSID	51	.036	.098	.179	8
THETA LIBR 230	.021	.067 .1	55 3 68 15	GAMMA CAS: L CEPHEID	2.0	144	.205	.280	41	TAU URSID	27 8•5	.050	.126 .133	.198	13
#APR URSID 10 G DRACONIO 44	·	.076 .1	39 3	AUG CEPH	13		.162 .171	.250 .251	15 30	PSI DRACO	64	.032	090 117	.164	8 9
ETA TAURID 52	.037		85 6 22 7	AUG DRACO AUG CANCR	7.3 11		.116	.176	8	B DRACONI OCT UMID	D 15		.095	.143	4
R DRACONID 20 GAMMA PEG 330U			94 5	PHI DRACO	8.6		.152 .120	.226 .194	23 13	ALP UR51D	35	.043	112	.194 .222	10 14
MAY PISCID 130	.038	.115 .2	42 B	AUG UMID E CAMELOP	20 9.1	078	.166	.250	15	A DRACONI OCT HERCU			.119	.193	10
EPS ARIET 19	.059		27 5	AUG URSID			.D71	.143	•	TALRIDS	8.0	064	.173	.255	- 2
MAY ARIET 20	,154		599 -99 164 4	AN DEL AG	y 9.	2 .064	.135	.202	10	*TRIANGUL			109	.159	. 5
#5 MAY OPH 73		.065 al	164 4	EP5 URSID	19		.159 .182	.239	22 31	C CEPHEID GAMPA TAU		D44	113	.194	10 11
*N MAY OPH 3.7 EPS AGUIL 53	053	145	266 1D	MU DRACO BETA URSI	2.1 D 8.1		.181	.267	14	KAPPA DRA			.231	.373	17
MAY URSID 9.9			232 15 236 7	GAMMA LEC	3.	1 .098	.161	.223	20 43	EPS DRACO		.041	132 201	.310	23
MAY DRACO 71	.031	.088	168 6	AN 1 AOUA CASS-SCEPH			. 1-13	.207	6	PHI TAURI	D 19	.033	.093	.176	5
MAY CASS 9.6			166 5 226 13	CASS-CEPH A CASSION			.171 ,138	.254 .236	11 12	IODTA AUR K CEPHEID		.018	150	.190	3 19
JUNE CAMEL 180	920.	.081	leo _6	X1 LEONID OMEGA CAS			.092	.174	9.	*DRACO-UR	15 5.6		.157	.244	15
PSI AURIG 6			221 21 172 5	E URSIUS	1.6			.187 .231	10	NCV DRACC 10DTA VIF		.010	.041 100	.196 193	3 10
JUHE AURIG 1		.101	156 5	F CAMELUF X1 DRACO) 1 2.				18	F CRACONI	D 70		.134	.219	11
#ZETA PERS 8.			483 90 218 6	SEPT LYR	D 2.	3 .112			26 7	NDV CAMEL SIG.TAUR	0 160	.029	UVU	.195	5 14
#CPHIUCHID 3		090	154	ALP TRIAP TAU LEUNI		2 .047			16	#MCNDCER!	D 110		.113	199	٥
JUNE LYRIU	0 .041		213 4 253 12	D CEPHEIL	9.	3 .068	.144	.215	10	M DRACON	0 22	.048	117 226	.191 .319	12
JUGA NUL	8 .057 B .036	048	176 6	C CASSIDI RHO CEPH	, 21	4 .055			7 5	AMI. GEMIP	()		170	255	24
ASCOH-SGR 2	4 .077	.164 •	255 16 181 17	CASS-CAM	L 5	5 .035	, .097	.178	6	#CHI DRIC	M 5.8	.100	,142	.27/	75
#51GKA CAP 6.	1 062	120	174 9	CEPHEID BETA UMI	3 18	0 .025			19	T VINIU	,		124 100	.184	5
	22 045	.131	199 9 179 B	CCAMELO	- 11	0 .026	.077	.158	7	DEC LYNCI ADLL DRAC	0 21		.114	.185	7
	/2 053		211 9	RHO URSI	. 3	5 ,041	•107	-185	6	- 					

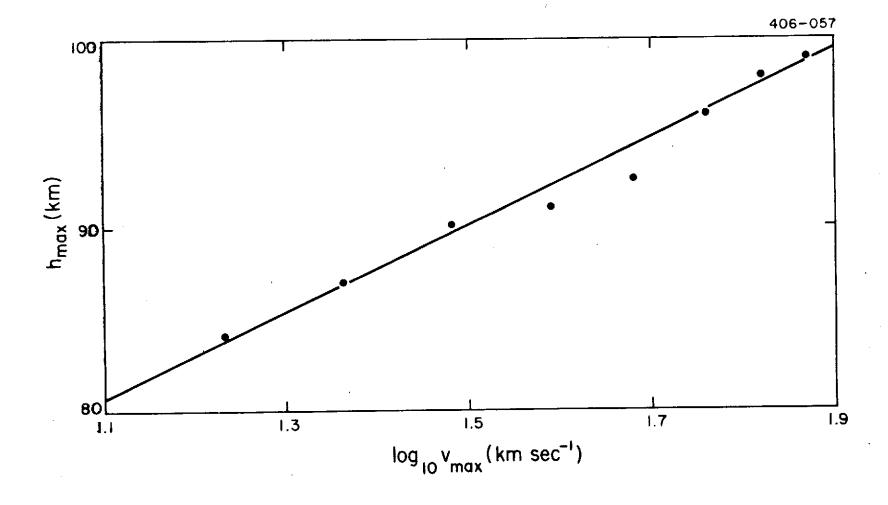


Figure 1. Mean heights at maximum ionization of 11061 meteors, with estimated corrections for diffusion.

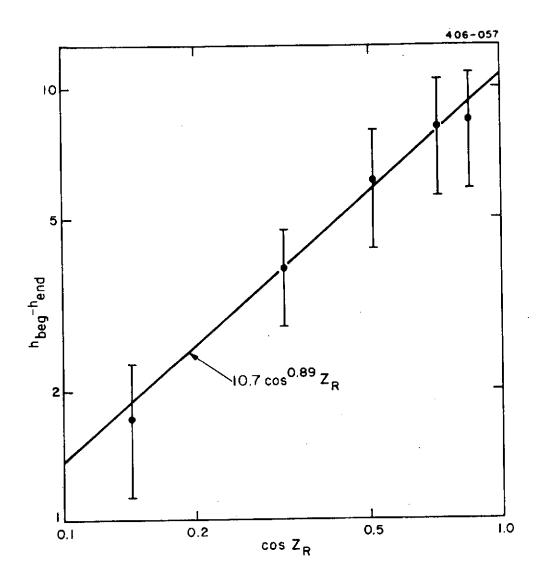


Figure 2. Vertical trail lengths and radiant zenith distances, from Table 5.

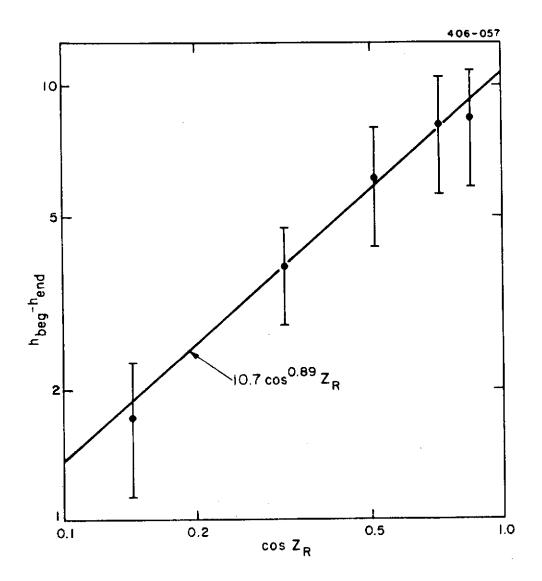


Figure 2. Vertical trail lengths and radiant zenith distances, from Table 5.